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Ejectors and jet pumps: Computer program for design and performance for compressible gas flow

Associated software: ESDUpac A9242

Endorsed by
The Institution of Chemical Engineers
The Institution of Mechanical Engineers

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THE PREPARATION OF THIS DATA ITEM

The work on this particular Data Item was monitored and guided by the Internal Flow Panel, which first met in 1979 and had the following membership:

Chairman	
Dr J.A. Eaton	— University College Galway, Ireland
Members	
Mr D.A. Campbell	— Rolls-Royce Ltd, Derby
Mr J. Campbell	— Ove Arup and Partners
Dr C.J. Clark	— BP International Ltd
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Prof. D.H. Freeston *	— Auckland University, New Zealand
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Prof. J.L. Livesey	— University of Salford
Dr M. Moore	— Independent
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* Corresponding Member

This Item supersedes and incorporates the methods of ESDU 84029 and 88002. The work on ESDU 84029, for the design and performance of ejectors and jet pumps with compressible air flows, was monitored and guided in 1984 by the following Working Party[†]:

Mr J. Campbell	— Babcock Power Ltd
Dr D.J. Cockrell	— University of Leicester
Mr J.S. Drabble	— Royal Aircraft Establishment (Pyestock)
Dr R.S. Silvester	— British Hydromechanics Research Association
Mr A.W. Wakefield	— Wakefield and Imberg
Mr R. Whitaker	— British Aerospace (Warton).

The initial assessment of the available information on compressible air flows in ejectors and jet pumps and the subsequent development of ESDU 84029 was undertaken (under contract to ESDU) by[†]

Ms A.E. Gibson	— Atkins Research and Development
Dr S.J. Murray	— Atkins Research and Development.

(Continued on inside back cover)

[†] Affiliations at the time are given

EJECTORS AND JET PUMPS COMPUTER PROGRAM FOR DESIGN AND PERFORMANCE FOR COMPRESSIBLE GAS FLOW

ESDU 92042 describes a computer program for the design of gas ejectors and jet pumps to meet given requirements and for prediction of performance.

Two design methods are provided. A 'quick' method is based on data from a range of typical single nozzle ejectors and requires a minimum of input data. A detailed design method is also provided (based on a one-dimensional flow theory given in the Appendix) which enables a more detailed assessment of the effects of internal losses to be made. This method may also be applied to multi-nozzle or annular nozzle designs. The performance prediction method is also based on the one-dimensional theory and calculates the flow conditions throughout the ejector given the dimensions, loss factors and entry flow conditions. The use of the program is illustrated by three worked examples. The program is provided to run within ESDUview, a user-friendly environment for personal computer users. An executable version of this program is available.

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EJECTORS AND JET PUMPS

Computer Program for Design and Performance for Compressible Gas Flow

1. NOTATION AND UNITS

Any consistent system of units may be used in the equations in this Item.*

		<i>Units</i>	
		<i>SI</i>	<i>British</i>
A	cross-sectional area	m^2	ft^2
A_{ME}	area ratio: A_4/A_e	—	—
A_R	area ratio: A_4/A'_e	—	—
A_R^*	area ratio: A_4/A_{th}	—	—
a	sonic velocity	m/s	ft/s
C_D	primary-nozzle discharge coefficient	—	—
d	diameter	m	ft
i	defines user estimated parameter	—	—
K	mixing duct momentum loss factor	—	—
L	length of mixing duct	m	ft
L_d	length of contraction or diffuser	m	ft
M	Mach number: V/a	—	—
$\dot{m}$	mass flow rate	kg/s	$\text{slug/s}^\dagger$
n	number of user estimates of parameter, number of nozzles	—	—
PP	primary parameter: $C_D(p'_{te}/p''_{te})/A_R$	—	—
p_t	absolute total pressure	$^\ddagger\text{kPa}$	lbf/ft^2
R	gas constant (for air, $R \approx 287 \text{ J/kg K}$, $3090 \text{ ft lbf/slug K}$)	J/kg K	$\text{ft lbf/slug K}^\dagger$
r_m	mass flow ratio: $\dot{m}''/\dot{m}'$	—	—
S	length of mixing duct entry	m	ft
SP	secondary parameter: $(p''_{te}/p_4)(A_R - 1)/A_R$	—	—

For footnotes see end of Notation Section.

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T_t	absolute total temperature	K	K
V	stream velocity	m/s	ft/s
γ	ratio of specific heat capacity at constant pressure to that at constant volume (for air, $\gamma \approx 1.4$)	—	—
η_d	contraction or diffuser total-pressure recovery: p_{t5}/p_{t4}	—	—
η_i	secondary flow inlet efficiency: p_{te}''/p_{t0}	—	—
ϕ_d	contraction or diffuser wall angle	degrees	degrees
ϕ_m	mixing duct wall equivalent angle	degrees	degrees

* For many parameters ESDUpac A9242 uses non-consistent, but more commonly-used, units to simplify the use of the program. The units required by the program are shown in Tables 5.1, 5.2, 5.3 and 5.4 and are displayed on-screen when running ESDUpac A9242 in ESDUview (see Section 4).

† 1 slug = 32.174 lb mass.

‡ 1 kPa = 1000 N/m²

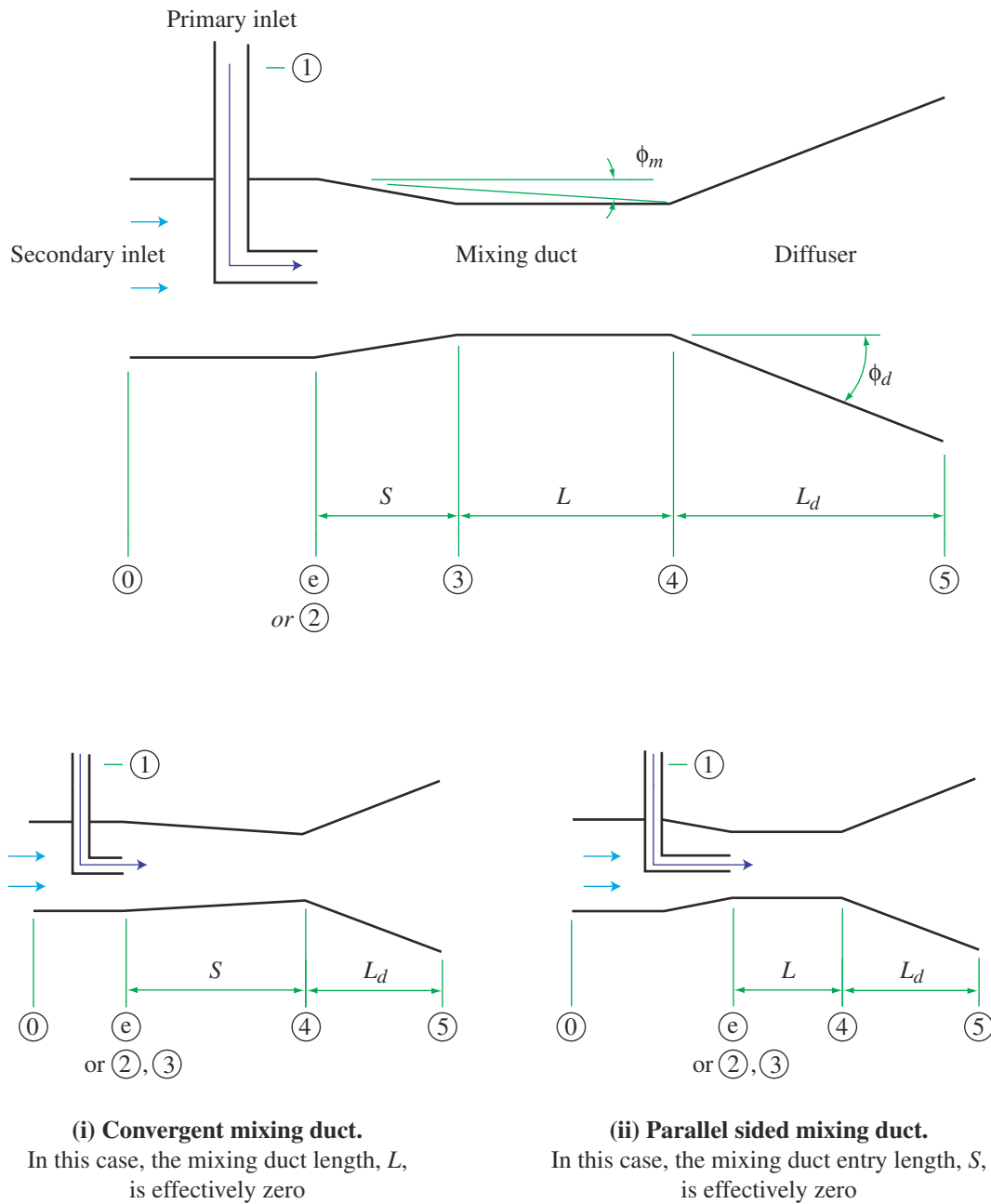
Subscripts

e	primary nozzle exit plane
th	primary nozzle throat
max	upper limit of parameter
0	secondary flow entry plane
1	primary nozzle entry plane
3	mixing duct entry plane
4	mixing duct exit plane
5	contraction or diffuser exit plane

The reference planes are defined in Sketch 1.1. Note that, for constant area mixing, planes 2 and 3 are coincident and are referred to by subscript e .

Superscripts

'	refers to primary stream or primary nozzle
''	refers to secondary stream or secondary inlet



Sketch 1.1 Ejector configuration and typical cases.