BS IEC 60076-8 : 1997 IEC 60076-8 : 1997

Power transformers — Application guide

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National foreword

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The UK participation in its preparation was entrusted to Technical Committee PEL/14, Power transformers, which has the responsibility to:

- aid enquirers to understand the text;
- present to the responsible international/European committee any enquiries on the interpretation, or proposals for change, and keep the UK interests informed;
- monitor related international and European developments and promulgate them in the UK.

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Summary of pages

This document comprises a front cover, an inside front cover, the IEC title page, pages 2 to 84, an inside back cover and a back cover.

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Transformateurs de puissance – Guide d'application

Power transformers – Application guide



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CONTENTS

		Page
FOF	REWORD	3
Clau	ise	
1	General	4
2	Characteristic properties of different three-phase winding combinations and magnetic circuit designs	5
3	Characteristic properties and application of auto-connected transformers	9
4	Zero-sequence properties – neutral load current and earth fault conditions, magnetic saturation and inrush current	13
5	Calculation of short-circuit currents in three-winding, three-phase transformers (separate winding transformers and auto-connected transformers) with earthed neutrals	26
6	Parallel operation of transformers in three-phase systems	41
7	Calculation of voltage drop for a specified load, three-winding transformer load loss	. 47
8	Specification of rated quantities and tapping quantities	63
9	Convertor applications with standard transformers	74
10	Guide to the measurement of losses in power transformers	76
Anr	nex A – Basic relations for single-phase and two-phase earth faults	. 83

INTERNATIONAL ELECTROTECHNICAL COMMISSION

POWER TRANSFORMERS – APPLICATION GUIDE

FOREWORD

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International Standard IEC 60076-8 has been prepared by IEC technical committee 14: Power transformers.

This first edition of IEC 60076-8 cancels and replaces IEC 60606 published in 1978. This edition constitutes a technical revision.

The text of this standard is based on the following documents:

FDIS	Report on voting
14/260/FDIS	14/297/RVD

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

IEC 60076 consists of the following parts, under the general title: Power transformers.

Part 1: 1993, General

Part 2: 1993, Temperature rise

Part 3: 1980, Insulation levels and dielectric tests

Part 5: 1976, Ability to withstand short circuit

Part 8: 1997, Application guide

Annex A is for information only.

POWER TRANSFORMERS – APPLICATION GUIDE

1 General

1.1 Scope and object

This Standard applies to power transformers complying with the series of publications IEC 60076.

It is intended to provide information to users about:

- certain fundamental service characteristics of different transformer connections and magnetic circuit designs, with particular reference to zero-sequence phenomena;

- system fault currents in transformers with YNynd and similar connections;

- parallel operation of transformers, calculation of voltage drop or rise under load, and calculation of load loss for three-winding load combinations;

- selection of rated quantities and tapping quantities at the time of purchase, based on prospective loading cases;

- application of transformers of conventional design to convertor loading;
- measuring technique and accuracy in loss measurement.

Part of the information is of a general nature and applicable to all sizes of power transformers. Several chapters, however, deal with aspects and problems which are of the interest only for the specification and utilization of large high-voltage units.

The recommendations are not mandatory and do not in themselves constitute specification requirements.

Information concerning loadability of power transformers is given in IEC 60354, for oilimmersed transformers, and IEC 60905, for dry-type transformers.

Guidance for impulse testing of power transformers is given in IEC 60722.

1.2 Normative references

The following normative documents contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of publication, the editions indicated were valid. All normative documents are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent edition of the normative documents indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

IEC 60050(421):1990, International Electrotechnical Vocabulary (IEV) – Chapter 421: Power transformers and reactors

IEC 60076: Power transformers

IEC 60076-1:1993, Power transformers – Part 1: General

IEC 60076-3:1980, Power transformers – Part 3: Insulation levels and dielectric tests

IEC 60289:1988, Reactors

IEC 60354:1991, Loading guide for oil-immersed power transformers

IEC 60722:1982, Guide to the lightning impulse and switching impulse testing of power transformers and reactors

IEC 60905:1987, Loading guide for dry-type power transformers

IEC 60909:1988, Short-circuit current calculation in three-phase a.c. systems

IEC 60909-1:1991, Short-circuit current calculation in three-phase a.c. systems – Part 1: Factors for the calculation of short-circuit currents in three-phase a.c. systems according to IEC 60909 (1988)

IEC 60909-2:1992, Electrical equipment – Data for short-circuit current calculations in accordance with IEC 60909 (1988)

IEC 61378-1: 1997, Convertor transformers – Part 1: Transformers for industrial applications

ISO 9001: 1994, Quality systems – Model for quality assurance in design, development, production, installation and servicing

2 Characteristic properties of different three-phase winding combinations and magnetic circuit designs

This chapter is an overview of the subject. Additional information is given in clause 4 on zero-sequence properties.

2.1 Y-, D-, and Z-connected windings

There are two principal three-phase connections of transformer windings: star (Y-connection) and delta (D-connection). For special purposes, particularly in small power transformers, another connection named zigzag or Z is also used. Historically, several other schemes have been in use (such as "truncated delta", "extended delta", "T-connection", "V-connection", etc.). While such connections are used in transformers for special applications, they no longer appear in common power transmission systems.

2.1.1 Advantages of a Y-connected winding

This type of winding:

- is more economical for a high-voltage winding;
- has a neutral point available;
- permits direct earthing or earthing through an impedance;
- permits reduced insulation level of the neutral (graded insulation);
- permits the winding taps and tapchanger to be located at the neutral end of each phase;
- permits single-phase loading with neutral current (see 2.2 and 4.8).

2.1.2 Advantages of a D-connected winding

This type of winding:

- is more economical for a high-current, low-voltage winding;

- in combination with a star-connected winding, reduces the zero-sequence impedance in that winding.

2.1.3 Advantages of a Z-connected winding

This type of winding:

- permits neutral current loading with inherently low zero-sequence impedance. (It is used for earthing transformers to create an artificial neutral terminal of a system);

- reduces voltage unbalance in systems where the load is not equally distributed between the phases.

2.2 Characteristic properties of combinations of winding connections

The notation of winding connections for the whole transformer follows the conventions in IEC 60076-1, clause 6.

This subclause is a summary of the neutral current behaviour in different winding combinations. Such conditions are referred to as having "zero-sequence components" of current and voltage. This concept is dealt with further in clauses 4 and 5.

The statements are also valid for three-phase banks of single-phase transformers connected together externally.

2.2.1 YNyn and YNauto

Zero-sequence current may be transformed between the windings under ampere-turn balance, meeting low short-circuit impedance in the transformer. System transformers with such connections may in addition be provided with delta equalizer winding (see 4.7.2 and 4.8).

2.2.2 YNy and Yyn

Zero-sequence current in the winding with earthed neutral does not have balancing ampereturns in the opposite winding, where the neutral is not connected to earth. It therefore constitutes a magnetizing current for the iron core and is controlled by a zero-sequence magnetizing impedance. This impedance is high or very high, depending on the design of the magnetic circuit (see 2.3). The symmetry of the phase-to-neutral voltages will be affected and there may be limitations for the allowable zero-sequence current caused by stray-flux heating (see 4.8).

2.2.3 YNd, Dyn, YNyd (loadable tertiary) or YNy + d (non-loadable delta equalizer winding)

Zero-sequence current in the star winding with earthed neutral causes compensating circulating current to flow in the delta winding. The impedance is low, approximately equal to the positive-sequence short-circuit impedance between the windings.

If there are two star windings with earthed neutrals (including the case of auto-connection with common neutral), there is a three-winding loading case for zero-sequence current. This is dealt with in 4.3.2 and 4.7.2, and in clause 5.

2.2.4 Yzn or ZNy

Zero-sequence current in the zigzag winding produces an inherent ampere-turn balance between the two halves of the winding on each limb, and provides a low short-circuit impedance.

2.2.5 Three-phase banks of large single-phase units – use of delta connected tertiary windings

In some countries, transformers for high-voltage system interconnection are traditionally made as banks of single-phase units. The cost, mass, and loss of such a bank is larger than for a corresponding three-phase transformer (as long as it can be made). The advantage of the bank concept is the relatively low cost of providing a spare fourth unit as a strategic reserve. It may also be that a corresponding three-phase unit would exceed the transport mass limitation.

The three single-phase transformers provide independent magnetic circuits, representing high magnetizing impedance for a zero-sequence voltage component.

It may be necessary to provide a delta equalizer winding function in the bank, or there may be a need for auxiliary power at relatively low-voltage from a tertiary winding. This can be achieved by external busbar connection from unit to unit in the station. The external connection represents an additional risk of earth fault or short circuit on the combined tertiary winding of the bank.

2.3 Different magnetic circuit designs

The most common magnetic circuit design for a three-phase transformer is the three-limb coreform (see figure 1). Three parallel, vertical limbs are connected at the top and bottom by horizontal yokes.

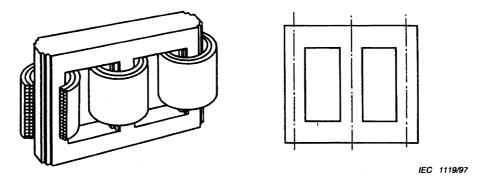


Figure 1 – Three-limb, core-form magnetic circuit

The five-limb, core-form magnetic circuit (see figure 2) has three limbs with windings and two unwound side limbs of lesser cross-section. The yokes connecting all five limbs also have a reduced cross-section in comparison with the wound limbs.

Page 8 BS IEC 60076-8 : 1997

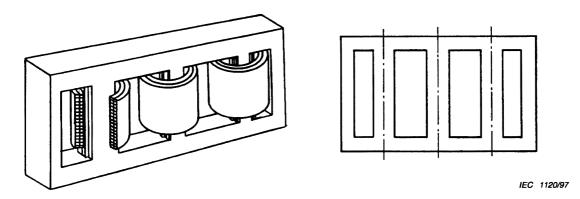
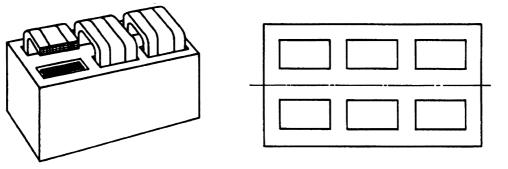


Figure 2 – Five-limb, core-form magnetic circuit

The conventional shell-form three-phase design has a frame with the three wound limbs horizontal and having a common centre line (see figure 3). The core-steel limbs inside the windings have an essentially rectangular cross-section and the adjoining parts of the magnetic circuit surround the windings like a shell.



IEC 1121/97

Figure 3 – Three-phase conventional shell-form magnetic circuit

A new three-phase shell-form magnetic circuit is the seven-limb core, in which the wound limbs are oriented in a different way (see figure 4).

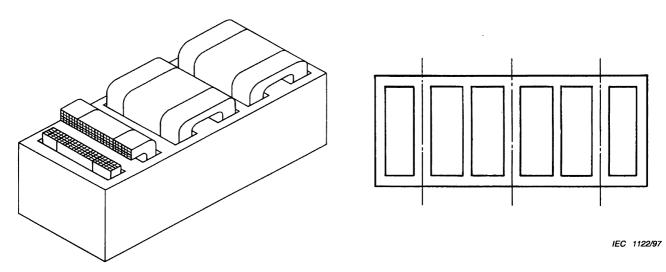


Figure 4 – Three-phase seven-limb shell-form magnetic circuit

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