# SUPPLEMENTARY READING LIST

- Adam, G., and T. A. Siewert. 1990. Sensing of GMAW droplet transfer modes using an ER100S-1 electrode. *Welding Journal* 69(3): 103-s–108-s.
- Aldenhoff, B. J., J. B. Stearns, and P. W. Ramsey. 1974. Constant potential power sources for multiple operation gas metal arc welding. *Welding Journal* 53(7): 425–429.
- Althouse, A. D., C. H. Turnquist, W. A. Bowditch, and K. E. Bowditch. 1984. *Modern welding*. South Holland, Illinois: The Goodheart-Willcox Company.
- Altshuller, B. 1998. A guide to GMA welding of aluminum. *Welding Journal* 77(6): 49.
- Baujet, V., and C. Charles. 1990. Submarine hull construction using narrow-groove GMAW. Welding Journal 69(8): 31–36.
- Bosworth, M. R. 1991. Effective heat input in pulsed current gas metal arc welding with solid wire electrodes. *Welding Journal* 70(5): 111-s-117-s.
- Bruss, R. A. 1996. Designing GMA welding guns with the welder's comfort in mind. *Welding Journal* 75(10): 31–33.
- Butler, C. A., R. P. Meister, and M. D. Randall. 1969. Narrow gap welding—a process for all positions. Welding Journal 48(2): 102–108.
- Cary, H. B. 1994. *Modern welding technology*. 3rd ed. Englewood Cliffs, New Jersey: Regents Prentice-Hall.
- Castner, H. R. and R. Singh. 1997. Pulsed vs. steady current GMAW: Which is louder? *Welding Journal* 76(11): 39–51.
- Castner, H. R. 1995. Gas metal arc welding fume generation using pulsed current. *Welding Journal* 74(2): 59-s-68-s.
- Chandiramani, D. 1994. Hydrogen reduced in wet underwater GMA welds. *Welding Journal* 73(3): 45– 49.
- Choi, S. K., C. D. Yoo, and Y. S. Kim. 1998. Dynamic simulation of metal transfer in GMAW, Part 1: Globular and spray transfer modes. *Welding Journal* 77(1): 38-s-44-s.
- Choi, S. K., C. D. Yoo, and Y. S. Kim. 1998. Dynamic simulation of metal transfer in GMAW, Part 2: Short-circuit transfer mode. Welding Journal 77(1): 45-s-51-s.
- DeSaw, F. A., and J. E. Rodgers. 1981. Automated welding in restricted areas using a flexible probe gas metal arc welding torch. *Welding Journal* 60(5): 17–22.
- Dillenbeck, V. R., and L. Castagno. 1987. The effects of various shielding gases and associated mixtures in

GMA welding of mild steel. Welding Journal 66(9): 45–49.

- DiPietro, D., and J. Young. 1996. Pulsed GMAW helps John Deere meet fume requirements. *Welding Journal* 75(10): 57–58.
- Dorling, D. V., A. Loyer, S. N. Russell, and T. S. Thompson. 1992. Gas metal arc welding used on mainline 80 ksi pipeline in Canada. *Welding Journal* 71(5): 55–61.
- Eickhoff, S. T., and T. W. Eagar. 1990. Characterization of spatter in low-current GMAW of titanium alloy plate. *Welding Journal* 69(10): 382-s–388-s.
- Fang, C. K., E. Kannatey-Asibu, Jr., and J. R. Barber. 1995. Acoustic emission investigation of cold cracking in gas metal arc welding of AISI 4340 steel. Welding Journal 74(6): 177-s–184-s.
- Farson, D., C. Conrardy, J. Talkington, K. Baker, T. Kershbaumer and F. Edwards. 1998. Arc initiation in gas metal arc welding. *Welding Journal* 77(8): 315-s– 321-s.
- Feree, S. E. 1995. New generation of cored wires creates less fume and spatter. *Welding Journal* 74(12): 45–49.
- French, I. E., and M. R. Bosworth. 1995. A comparison of pulsed and conventional welding with basic flux cored and metal cored welding wires. *Welding Journal* 74(6): 197-s–205-s.
- Hilton, D. E., and J. Norrish. 1988. Shielding gases for arc welding. *Welding and Metal Fabrication* 189– 196.
- Hussain, H. M., P. K. Ghosh, P. C. Gupta, and N. B. Potluri. 1996. Properties of pulsed current multipass GMA welded Al-Zn-Mg alloy. *Welding Journal* 75(7): 209-s-215-s.
- Irving, B. 1997. GMA welding goes to work on the Z3 Roadster's exhaust system. *Welding Journal* 76(2): 29–33.
- Irving, B. 1993. Laser beam and GMA welding lines go on-stream at Arvin Industries, *Welding Journal* 72(11): 47–50.
- Irving, B. 1992. Inverter power sources cut fume emissions in GMAW. Welding Journal 71(2): 53–57.
- Johnson, J. A, N. M. Carlson, H. B. Smartt, and D. E. Clark. 1991. Process control of GMAW: Sensing of metal transfer mode. *Welding Journal* 70(4): 91-s-99-s.
- Jonsson, P. G., A. B. Murphy, and J. Szekely. 1995. The influence of oxygen additions on argon-shielded gas metal arc welding processes. *Welding Journal* 74(2): 48-s–58-s.
- Jonsson, P. G., J. Szekely, R. B. Madigan, and T. P. Quinn. 1995. Power characteristics in GMAW: Experimental and numerical investigation. *Welding Journal* 74(3): 93-s-102-s.
- Kim, J. W., and S. J. Na. 1995. A study on the effect of contact tube-to-workpiece distance on weld bead

shape in gas metal arc welding. *Welding Journal* 74(5): 141-s-152-s.

- Kim, J. W., and S. J. Na. 1993. A self-organizing fuzzy control approach to arc sensor for weld joint tracking in gas metal arc welding of butt joints. *Welding Journal* 72(2): 60-s–66-s.
- Kim, J. W., and S. J. Na. 1991. A study on an arc sensor for gas metal arc welding of horizontal fillets. *Welding Journal* 70(8): 216-s–221-s.
- Kim, Y. S., and T. W. Eagar. 1993. Metal transfer in pulsed current GMAW. *Welding Journal* 72(7): 279-s-287-s.
- Kim, Y. S., and T. W. Eagar. 1993. Analysis of metal transfer in gas metal arc welding. *Welding Journal* 72(6): 269-s-278-s.
- Kim, Y. S., D. M. McEligot, and T. W. Eagar. 1991. Analysis of electrode heat transfer in gas metal arc welding. *Welding Journal* 70(1): 20-s–31-s.
- Kimura, S., I. Ichihara and Y. Nagai. 1979. Narrow-gap gas metal arc welding process in flat position. *Weld-ing Journal* 58(7): 44–52.
- Kiyohara, M., T. Okada, Y. Wakino and H. Yamamoto. 1977. On the stabilization of GMA welding of aluminum. *Welding Journal* 56(3): 20–28.
- Kjeld. F. 1990. Gas metal arc welding for the collision repair industry. *Welding Journal* 69(4): 39.
- Kluken, A. O., and B. Bjorneklett. 1997. A study of mechanical properties for aluminum GMA weldments. Welding Journal 76(2): 39–44.
- Lesnewich, A. 1991. Technical commentary: Observations regarding electrical current flow in the gas metal arc. *Welding Journal* 70(7): 171-s–172-s.
- Lesnewich, A. *MIG welding with pulsed power*. 1972. Welding Research Council Bulletin 170. New York; Welding Research Council.
- Lesnewich, A. 1958. Control of melting rate and metal transfer in gas-shielded metal-arc welding. *Welding Journal* 37(8): 343–353.
- Lincoln Electric Company, The. 1994. *The procedure handbook of arc welding*. 13th ed. Cleveland, Ohio: The Lincoln Electric Company.
- Lincoln Electric Company, The. 1992. Switch to metal cored electrodes helps crane fabricator gain productivity. *Welding Journal* 71(6): 75–77.
- Liu, S., and T. A. Siewart. 1989. Metal transfer in gas metal arc welding: Droplet rate. *Welding Journal* 68(2): 52-s-58-s.
- Lu, M. J., and S. Kou. 1989. Power inputs in gas metal arc welding of aluminum. Part 2. *Welding Journal* 68(11): 452-s-456-s.
- Lu, M. J., and S. Kou. 1989. Power inputs in gas metal arc welding of aluminum. Part 1. *Welding Journal* 68(9): 382-s-388-s.
- Lyttle, K. A. 1983. GMAW—A versatile process on the move. *Welding Journal* 62(3): 15–23.

- Lyttle, K. A. 1982. Reliable GMAW means understanding wire quality, equipment and process variables. *Welding Journal* 61(3): 43–48.
- Malin, V. Y. 1983. The state-of-the-art of narrow gap welding, Part II. Welding Journal 62(6): 37–46.
- Malin, V. Y. 1983. The state-of-the-art of narrow gap welding, Part I. Welding Journal 62(4): 22–30.
- Manz, A. F. 1990. The dawn of gas metal arc welding. Welding Journal 69(1): 67–68.
- Manz, A. F. 1973. *The welding power handbook*. Miami: American Welding Society.
- Manz, A. F. 1969. Inductance vs. slope for control for gas metal arc power. *Welding Journal* 48(9): 707–712.
- Mitchie, K., S. Blackman, and T. E. B. Ogunbiyi. 1999. Twin-wire GMAW: process characteristics and applications. *Welding Journal* 78(5): 31–34.
- Miyazaki, H., H. Miyauchi, Y. Sugiyama, and T. Shinoda. 1994. Puckering phenomenon and its prevention in GMA welding of aluminum alloys. *Welding Journal* 73(12): 277-s-284s.
- Modensi, P. J., and J. H. Nixon. 1994. Arc instability phenomena in GMA welding. *Welding Journal* 73(9): 219-s-224-s.
- Morris, R. W. 1968. Application of multiple electrode gas metal arc welding to structural steel fabrication. *Welding Journal* 47(5): 379–385.
- Nadeau, F. 1990. Computerized system automates GMA pipe welding. *Welding Journal* 69(6): 53–59.
- Occupational Safety and Health Administration (OSHA). 1999. Occupational safety and health standards for general industry. In Code of Federal Regulations (CFR), Title 29 CFR 1910, Subpart Q. Washington D.C.: Superintendent of Documents, U.S. Government Printing Office.
- Ohring, S. and H. J. Lugt. 1999. Numerical simulation of a time-dependent 3-D GMA weld pool due to a moving arc. *Welding Journal* 78(12): 416-s-424-s.
- Pan, J. L., R. H. Zhang, Z. M. Ou, Z. Q. Wu and Q Chen. 1989. Adaptive control GMA welding—A new technique for quality control." Welding Journal 68(3): 73–76.
- Pierre, E. R. 1985. Welding processes and power sources. 3rd ed. Minneapolis: Burgess Publishing Company.
- Quinn, T. P., C. Smith, C. N. McGowan, E. Blachowiak, and R. B. Madigan. 1999. Arc sensing for defects in constant-voltage gas metal arc welding. *Welding Journal* 78(9): 322-s–328-s.
- Quinn, T. P., R. B. Madigan, and T. A. Siewert. 1994. An electrode extension model for gas metal arc welding. *Welding Journal* 73(10) 241-s–248-s.
- Quinn, T. P., R. B. Madigan, M. A. Mornis, and T. A. Siewert. 1995. Contact tube wear detection in gas metal arc welding. *Welding Journal* 74(4): 141-s-121-s.

- Rajasekaran, S. 1999. Weld bead characteristics in pulsed GMA welding of Al-Mg alloys, *Welding Journal* 78(12): 416-s-424-s.
- Rajasekaran, S., S. D. Kulkarn, U. D. Mallya, and R. C. Chaturvedi. 1998. Droplet detachment and plate fusion characteristics in pulsed current gas metal arc welding. *Welding Journal* 77(6): 254-s–268-s.
- Reilly. R. 1990. Real-time weld quality monitor controls GMA welding. *Welding Journal* 69(3): 36.
- Rhee, S., and E. Kannatey-Asibu, Jr. 1992. Observation of metal transfer during gas metal arc welding. *Welding Journal* 71(10): 381-s–386-s.
- Richardson, I. M., P. W. Bucknall, and I. Stares. 1994. The influence of power source dynamics on wire melting rate in pulsed GMA welding. *Welding Journal* 73(2): 32-s–37-s.
- Sadler, H. 1999. A look at the fundamentals of gas metal arc welding. *Welding Journal* 78(5): 45–47.
- Sampath, K., R. S. Green, D.A. Civis, B. E. Williams, and P. J. Konkol. 1995. Metallurgical model speeds development of GMA welding wire for HSLA steel. *Welding Journal* 74(12): 69–76.
- Shackleton, D. N., and W. Lucas. 1974. Shielding gas mixtures for high quality mechanized GMA welding of Q and T steels. *Welding Journal* 53(12): 537-s-547-s.

- Smartt, H. B., and C. J. Einerson. 1993. A model for mass input control in gas metal arc welding. Welding Journal 72(5): 217-s–229-s.
- Stanzel, K. 1999. Nothing complicated—Just basic GMA welding. *Welding Journal* 78(5): 36–38.
- Sullivan, D. 1998. The gas metal arc welding process celebrates a 50th anniversary. *Welding Journal* 77(9): 53–54.
- Tekriwal, P., and J. Mazumder. 1988. Finite element analysis of three-dimensional transient heat transfer in GMA welding. *Welding Journal* 67(7): 150-s–156-s.
- Tsao, K. C., and C. S. Wir. 1988. Fluid flow and heat transfer in GMA weld pools. *Welding Journal* 67(3): 70-s–75-s.
- Union Carbide Corporation. 1984. *MIG Welding handbook*. Danbury, Connecticut: Union Carbide Corporation, Linde Division.
- Villafuerte, J. 1999. Understanding contact tip longevity for gas metal arc welding. *Welding Journal* 78(12): 29–35.
- Waszink, J. H., and G. J. P. M. Van Den Heurel. 1982. Heat generation and heat flow in the filler metal in GMA welding. *Welding Journal* 61(8): 269-s–282-s.
- Zhu, P., M. Rados, and S. W. Simpson. 1997. Theoretical predictions of the start-up phase in GMA welding. *Welding Journal*, 76(7): 269-s–274-s.

# **CHAPTER 5**

# FLUX CORED ARC WELDING



#### Prepared by the Welding Handbook Chapter Committee on Flux Cored Arc Welding:

**D. B. Arthur, Chair** *J. W. Harris Company* 

**B. A. Morrett** *ITW/Hobart Brothers Company* 

J. E. Beckham ThermoKing-Ingersoll Rand

**D. Sprenkel** Consultant

#### Welding Handbook Committee Member:

**C. E. Pepper** ENGlobal Engineering, Inc.

#### Contents

Introduction	210
Fundamentals	210
Applications	211
Equipment	215
Materials	219
Process Control	237
Joint Designs and Welding Procedures	241
Weld Quality	247
Troubleshooting	247
Economics	247
Safe Practices	250
Conclusion	252
Bibliography	252
Supplementary Reading List	253

# **CHAPTER 5**

# FLUX CORED ARC WELDING

# INTRODUCTION

Flux cored arc welding (FCAW) is a welding process that uses an arc between a continuous filler metal electrode and the weld pool. The process is used with shielding from a flux contained within the tubular electrode, with or without additional shielding from an externally supplied gas, and without the application of pressure.<sup>1,2</sup>

The remarkable operating characteristics and weld properties that distinguish FCAW from other arc welding processes are attributable to the continuously fed flux cored electrode. The tubular electrode is a filler metal composite consisting of a metal sheath and a core of various powdered materials manufactured in the form of wire. During welding, an extensive protective slag cover is produced on the face of the weld bead.

Flux cored arc welding offers two major variations, self-shielded (FCAW-S) and gas-shielded (FCAW-G), which add great flexibility to the process. These variations differ in the method of shielding the arc and weld pool from atmospheric contamination (oxygen and nitrogen).

Flux cored arc welding is an efficient welding process readily adaptable to semiautomatic or automatic welding operations and capable of producing high-quality weld metal at a high deposition rate. Many industries rely on flux cored arc welding to produce high-integrity welds. Users of the process include manufacturers or builders of pressure vessels, submarines, aircraft carriers, earth-moving equipment, and buildings and other structures.

This chapter covers the fundamental operating principles of the flux cored arc welding process and describes the necessary equipment and materials. Significant information is included for a variety of flux cored electrodes used in the major applications of FCAW. Welding procedures, process control, and weld quality are discussed. The chapter ends with comments on the economics of the process and important information on safe practices.

# **FUNDAMENTALS**

The history of gas-shielded arc welding provides the background for the technology and evolution of flux cored arc welding. Gas-shielded metal arc welding processes have been in use since the early 1920s, when it was demonstrated that a significant improvement of weld metal properties could be produced if the arc and molten weld metal were protected from atmospheric contamination. However, the development of covered electrodes in the late 1920s diminished interest in gasshielding methods. Interest was renewed in the early 1940s with the introduction and commercial acceptance of gas tungsten arc welding (GTAW) and, later in the same decade, gas metal arc welding (GMAW). Argon and helium were the two primary shielding gases used at that time.

Research conducted on manual welds made with covered electrodes focused on the analysis of the gas produced in the disintegration of electrode coverings. Results confirmed that carbon dioxide  $(CO_2)$  was the predominant gas given off by electrode coverings. This

<sup>1.</sup> American Welding Society (AWS) Committee on Definitions and Symbols, 2001, *Standard Welding Terms and Definitions*, A3.0:2001, Miami: American Welding Society.

<sup>2.</sup> At the time of preparation of this chapter, the referenced codes and other standards were valid. If a code or other standard is cited without a date of publication, it is understood that the latest edition of the document referred to applies. If a code or other standard is cited with the date of publication, the citation refers to that edition only, and it is understood that any future revisions or amendments to the code or standard are not included. As codes and standards undergo frequent revision, the reader is advised to consult the most recent edition.

discovery quickly led to the use of  $CO_2$  as a shielding gas for welds made on carbon steels with GMAW. Although early experiments with  $CO_2$  were unsuccessful, techniques were eventually developed which permitted its use. Gas metal arc welding using  $CO_2$  became available in the mid-1950s.

In concurrent research,  $CO_2$  shielding was combined with a flux-containing tubular electrode, which overcame many of the problems previously encountered. Operating characteristics were improved by the addition of the core materials, and weld quality was improved by eliminating atmospheric contamination. These experiments resulted in the development of flux cored arc welding. This new process was introduced at the American Welding Society (AWS) Exposition in Buffalo, New York, in 1954. By 1957 the electrodes and equipment were refined, and the process was introduced commercially in essentially its present form.

During the 1990s significant improvements were made in both gas-shielded and self-shielded electrode arc stability that resulted in much less spatter than the earlier electrodes produced. The impact resistance of FCAW electrodes was also significantly improved. The development and production of alloy electrodes and small-diameter electrodes, down to 0.8 millimeters (mm) (0.030 inches [in.]), were other advances.

Improvements continue to be made to the FCAW process. Modern power sources and electrode (wire) feeders are greatly simplified and more dependable than their predecessors. Welding guns are lightweight and rugged, and electrodes undergo continuous improvement.

### PROCESS VARIATIONS

The two major variations of the FCAW process, the self-shielded and the gas-shielded versions, are shown in Figure 5.1. Both illustrations in Figure 5.1 emphasize the melting and deposition of filler metal and flux and show the formation of a slag covering the weld metal. Cross sections of examples of FCAW electrodes also are shown in Figure 5.1.

In the gas-shielded method, the shielding gas ( $CO_2$  or a mixture of argon and  $CO_2$ ) protects the molten metal from the oxygen and nitrogen present in air by forming an envelope of gas around the arc and over the weld pool. Little need exists for denitrification of the weld metal because air is mostly excluded, along with the nitrogen it contains. However, some oxygen may be generated from the dissociation of  $CO_2$ , which forms carbon monoxide and oxygen. The compositions of the electrodes are formulated to provide deoxidizers that combine with small amounts of oxygen in the gas shield.

Self-shielded flux cored arc welding is often the process of choice for field welding because it can tolerate stronger air currents than the gas-shielded variation. The main reason for this distinction is that some shielding is provided by the high-temperature decomposition of some of the electrode core ingredients. The vaporization of these ingredients displaces air from the area immediately surrounding the arc. In addition, the wire contains a large proportion of scavengers (deoxidizers and denitrifiers) that combine with undesirable elements that might contaminate the weld pool. A slag cover protects the metal from the air surrounding the weld.

## **APPLICATIONS**

Both self-shielded and gas-shielded flux cored arc welding can be used in most welding applications. However, the specific characteristics of each method make each suitable for different operating conditions. The process is used to weld carbon- and low-alloy steels, stainless steels, cast irons, and nickel and cobalt alloys. It is also used for the arc spot welding of lap joints in sheet and plate, as well as for cladding and hardfacing.

Flux cored arc welding is widely used in fabrication shops, for maintenance applications, and in field erection work. An example of field erection work is shown in Figure 5.2, in which both self-shielded and gasshielded FCAW are used in the fabrication of an offshore oil drilling structure.

Flux cored arc welding can be used to produce weldments that conform to the ASME Boiler and Pressure Vessel Code,<sup>3</sup> the rules of the American Bureau of Shipping,<sup>4</sup> and Structural Welding Code—Steel, AWS D1.1.<sup>5</sup> The process is given prequalified status in AWS D1.1. Stainless steel, self-shielded, and gas-shielded flux cored electrodes are used in general fabrication, surfacing, joining dissimilar metals, and maintenance and repair.

Figure 5.3, which shows the fabrication of a suction filter used in the pulp and paper industry, illustrates the versatility of the FCAW process. The base material in this application was ST-360-C; E308LT1 electrodes were used.

The self-shielded method can often be used for applications that are normally welded with the shielded metal arc welding (SMAW) process. Gas-shielded FCAW can also be used for some applications that are welded by the GMAW process. The selection of selfshielded or gas-shielded FCAW depends on the type of electrodes available, the type of welding equipment available, the environment in which the welding is to be

<sup>3.</sup> American Society of Mechanical Engineers (ASME) Boiler and Pressure Vessel Code Committee, 1998, *Boiler and Pressure Vessel Code*. New York: American Society of Mechanical Engineers.

<sup>4.</sup> American Bureau of Shipping (ABS) Group, ABS Plaza, 166855 Northchase Drive, Houston, TX 77060-6008.

<sup>5.</sup> American Welding Society (AWS) Committee on Structural Welding, 2002, *Structural Welding Code—Steel*, AWS D1.1/D1.1M:2002, Miami: American Welding Society.



Figure 5.1—Self-Shielded and Gas-Shielded Flux Cored Arc Welding

done, the mechanical property requirements of the welded joints, and the joint design and fitup. The advantages and disadvantages of FCAW should be compared to those of other processes when it is evaluated for a specific application.

## **ADVANTAGES**

When compared to SMAW, higher productivity is the chief advantage of flux cored arc welding for many applications. This generally translates into lower overall costs per pound of metal deposited in joints that permit continuous welding and easy FCAW gun and equipment accessibility. The advantages are higher deposition rates, higher operating factors, and higher deposition efficiency (no stub loss).

In addition to the advantages of FCAW over the manual SMAW process, FCAW also provides certain advantages over submerged arc welding (SAW) and GMAW. In many applications, FCAW produces highquality weld metal at lower cost with less effort on the part of the welder than SMAW. Flux cored arc welding



Figure 5.2—Offshore Drilling Structure Fabricated with Self-Shielded and Gas-Shielded Flux Cored Arc Welding

is more forgiving of minor disparities in procedures and differences in welder skill than GMAW, and it is more flexible and adaptable than SAW. Among the benefits offered by FCAW are the following:

- 1. High-quality weld metal deposit,
- 2. Excellent weld appearance,
- 3. Welds many steels in a wide thickness range,
- 4. High operating factor and easily mechanized,
- 5. High deposition rate (up to four times greater than SMAW) and high current density,

- 6. Relatively high electrode deposit efficiency,
- 7. Allows economical engineering of joint designs,
- 8. Visible arc contributes to easy use,
- 9. Requires less precleaning than GMAW,
- 10. Often results in less distortion compared to SMAW,
- 11. Exceptionally good fusion when used with shielding gas compared to GMAW-S,
- 12. High tolerance for contaminants that may cause weld cracking,
- 13. Resistance to underbead cracking,



Photograph courtesy of Bohler Thyssen Welding USA, Inc.

#### Figure 5.3—Flux Cored Arc Welding of a Suction Filter Used in the Pulp and Paper Industry

- 14. Self-shielding characteristic of electrodes eliminates the need for flux handling and gas apparatus, and
- 15. Self-shielding tolerates windy conditions in outdoor applications. (See No. 6 relative to gas shields under "Limitations" in the next section).

An example of the good sidewall fusion, deep penetration and smooth weld profile that can be obtained with gas-shielded FCAW is shown in Figure 5.4

#### LIMITATIONS

Compared to the SMAW process, the major limitations of FCAW are the higher cost of the equipment, the relative complexity of setup and control of the equipment, and the restriction on operating distance from the electrode wire feeder. Flux cored arc welding may generate large volumes of welding fumes and requires suitable exhaust equipment, except in field work. Compared to the slag-free GMAW process, the need for removing slag between passes is an added labor cost when using FCAW. This is especially true in making root pass welds. However, in most cases, slag is easily removed and cleanup time is minimized, as shown in Figure 5.5. The limitations of FCAW are summarized as follows:

- 1. FCAW is limited to welding ferrous metals and nickel-base alloys;
- 2. The process produces a slag covering that must be removed;
- 3. FCAW electrode wire is more expensive on a weight basis than solid electrode wires, except for some high-alloy steels;
- 4. The equipment is more expensive and complex than that required for SMAW, however, increased productivity usually compensates for this;



Photograph courtesy of Bohler Thyssen Welding USA, Inc.

Figure 5.4—Flux Cored Arc Weld Profile



Photograph courtesy of Bohler Thyssen Welding USA, Inc.

Figure 5.5—Self-Peeling Slag Reveals a Clean Flux Cored Arc Weld

- 5. The wire feeder and power source must be fairly close to the point of welding;
- 6. For gas-shielded FCAW, the external shield may be adversely affected by breezes and drafts;
- 7. Equipment is more complex than that used for SMAW, so more maintenance is required; and
- 8. More smoke and fumes are generated by FCAW than by GMAW and SAW.

It should be noted that self-shielded FCAW is not adversely affected by windy conditions, except in very high winds, because the shield is generated at the end of the electrode exactly where it is required.

## EQUIPMENT

The basic equipment setup for flux cored arc welding is shown in Figure 5.6. Equipment consists of a power source, electrode feed and current controls, a shielding gas source, a wire electrode feeding system, a welding gun, and the associated cables and gas hoses. In addition, appropriate fume extraction equipment may be needed. Proper ventilation or some means of fume removal is necessary for FCAW.

### SEMIAUTOMATIC EQUIPMENT

Control equipment for semiautomatic self-shielded and gas-shielded flux cored arc welding is similar. The major difference between the shielding variations is the provision for supplying and metering gas to the arc of the electrode in the gas-shielded method.

#### **Power Source**

The recommended power source is the direct current (dc) constant-voltage type, similar to power sources used for GMAW. The power source should be capable of operating at the maximum current required for the specific application. Most semiautomatic applications use less than 500 amperes (A). The voltage control should be capable of adjustments in increments of one volt or less. Constant-current dc power sources of adequate capacity with appropriate controls and wire feeders are sometimes used, but applications are rare.

### **Electrode Feed Control**

The purpose of the electrode (wire) feed control is to supply the continuous electrode to the welding arc at a constant preset rate. The rate at which the electrode is fed into the arc determines the welding amperage supplied by a constant-voltage power source. If the