

Table 2-7W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5005 - H34	B209 0.009 to 1.000 in. thick
axial tension stress on net effective area	D.2b	7.7		
axial tension stress on gross area	D.2a	3.0		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	4.6	$F_{tyw} =$	5 k/in ²
<u>Bearing</u>			$F_{cyw} =$	5 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	15.4	$F_{tuw} =$	15 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	10.2	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	10.0	$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	3.0	23.4	$0.00001 \lambda^2 - 0.012\lambda + 3.3$	236	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2	-	see F.4	236	$60,414/\lambda^2$	
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	3.0	12.2	$3.7 - 0.056\lambda$	44	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	3.0	12.2	$3.7 - 0.056\lambda$	33.2	$61/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	3.0	38.0	$3.7 - 0.018\lambda$	104	$192/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	3.0	23.4	$3.2 - 0.009\lambda$	236	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	3.0	70.3	$3.8 - 0.086\lambda^{1/2}$	1066	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	3.0	60.9	$3.7 - 0.011\lambda$	166	$307/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	4.5	32.5	$4.9 - 0.011\lambda$	222	$544/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	4.5	6.0	$4.9 - 0.060\lambda$	55	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	4.5	72.8	$4.9 - 0.005\lambda$	497	$1,219/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$5.6 - 0.203\lambda^{1/2}$	259.1	$3.8 - 0.086\lambda^{1/2}$	1066	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	60.9	see B.5.5.5	221	$307/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	1.8	64.3	$2.2 - 0.007\lambda$	228	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	1.8	26.8	$2.2 - 0.016\lambda$	95	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	1.8	127.9	$2.9 - 0.009\lambda$	228	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	1.8	64.3	$2.2 - 0.007\lambda$	228	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-8W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5050 - H34	B209 0.009 to 0.249 in. thick
axial tension stress on net effective area	D.2b	9.2	5050 - H34	B210 0.010 to 0.500 in. thick
axial tension stress on gross area	D.2a	3.6		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	5.5	$F_{tyw} =$	6 k/in ²
<u>Bearing</u>			$F_{cyw} =$	6 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	18.5	$F_{tuw} =$	18 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	12.3	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	12.0	$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	3.6	23.2	$0.00001 \lambda^2 - 0.015\lambda + 4.0$	215	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2		-	see F.4	215	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	3.6	11.6	$4.5 - 0.075\lambda$	40	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	3.6	11.6	$4.5 - 0.075\lambda$	30.1	$68/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	3.6	36.3	$4.5 - 0.024\lambda$	94	$211/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	3.6	23.2	$3.9 - 0.012\lambda$	215	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	3.6	65.7	$4.5 - 0.111\lambda^{1/2}$	920	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	3.6	58.0	$4.5 - 0.015\lambda$	150	$339/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	5.5	34.0	$6.0 - 0.015\lambda$	201	$599/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	5.5	6.3	$6.0 - 0.080\lambda$	50	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	5.5	76.3	$6.0 - 0.007\lambda$	451	$1,343/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$6.8 - 0.261\lambda^{1/2}$	228.3	$4.5 - 0.111\lambda^{1/2}$	920	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	58.0	see B.5.5.5	201	$339/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	2.2	61.3	$2.7 - 0.009\lambda$	207	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	2.2	25.5	$2.7 - 0.021\lambda$	86	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	2.2	118.3	$3.5 - 0.011\lambda$	207	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	2.2	61.3	$2.7 - 0.009\lambda$	207	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_p/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-9W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5052 - H32	B209 0.017 to 2.000 in. thick
axial tension stress on net effective area	D.2b	12.8	5052 - H32	B210 0.010 to 0.450 in. thick
axial tension stress on gross area	D.2a	5.8		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	7.7	$F_{tyw} =$	9.5 k/in ²
<u>Bearing</u>			$F_{cyw} =$	9.5 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	25.6	$F_{tuw} =$	25 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	17.1	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	16.7	$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	5.8	22.6	$0.00003 \lambda^2 - 0.032\lambda + 6.5$	169	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2	-	see F.4		169	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	5.8	10.3	$7.4 - 0.156\lambda$	31	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	5.8	10.3	$7.4 - 0.156\lambda$	23.5	$87/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	5.8	32.1	$7.4 - 0.050\lambda$	74	$271/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	5.8	22.6	$6.3 - 0.025\lambda$	169	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	5.8	55.3	$7.3 - 0.210\lambda^{1/2}$	573	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	5.8	51.3	$7.4 - 0.031\lambda$	118	$433/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	8.6	36.1	$9.8 - 0.031\lambda$	157	$767/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	8.6	6.7	$9.8 - 0.167\lambda$	39	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	8.6	80.9	$9.8 - 0.014\lambda$	353	$1,719/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$11.0 - 0.494\lambda^{1/2}$	166.0	$7.3 - 0.210\lambda^{1/2}$	573	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	51.3	see B.5.5.5	157	$433/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	3.5	54.1	$4.4 - 0.018\lambda$	162	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	3.5	22.5	$4.4 - 0.044\lambda$	67	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	3.5	97.2	$5.8 - 0.024\lambda$	162	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	3.5	54.1	$4.4 - 0.018\lambda$	162	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$

† $k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-10W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5052 - H34	B209 0.009 to 1.000 in. thick
axial tension stress on net effective area	D.2b	12.8	5052 - H34	B210 0.010 to 0.450 in. thick
axial tension stress on gross area	D.2a	5.8		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	7.7	$F_{tyw} =$	9.5 k/in ²
<u>Bearing</u>			$F_{cyw} =$	9.5 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	25.6	$F_{tuw} =$	25 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	17.1	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	16.7	$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	5.8	22.6	$0.00003 \lambda^2 - 0.032\lambda + 6.5$	169	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2		-	see F.4	169	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	5.8	10.3	$7.4 - 0.156\lambda$	31	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	5.8	10.3	$7.4 - 0.156\lambda$	23.5	$87/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	5.8	32.1	$7.4 - 0.050\lambda$	74	$271/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	5.8	22.6	$6.3 - 0.025\lambda$	169	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	5.8	55.3	$7.3 - 0.210\lambda^{1/2}$	573	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	5.8	51.3	$7.4 - 0.031\lambda$	118	$433/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	8.6	36.1	$9.8 - 0.031\lambda$	157	$767/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	8.6	6.7	$9.8 - 0.167\lambda$	39	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	8.6	80.9	$9.8 - 0.014\lambda$	353	$1,719/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$11.0 - 0.494\lambda^{1/2}$	166.0	$7.3 - 0.210\lambda^{1/2}$	537	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	51.3	see B.5.5.5	157	$433/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	3.5	54.1	$4.4 - 0.018\lambda$	162	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	3.5	22.5	$4.4 - 0.044\lambda$	67	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	3.5	97.2	$5.8 - 0.024\lambda$	162	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	3.5	54.1	$4.4 - 0.018\lambda$	162	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_p/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-11W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5052 - H36	B209 0.006 to 0.162 in. thick
axial tension stress on net effective area	D.2b	12.8		
axial tension stress on gross area	D.2a	5.8		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	7.7	$F_{tyw} =$	9.5 k/in ²
<u>Bearing</u>				
bolts or rivets on holes	J.3.6a, J.4.6	25.6	$F_{cyw} =$	9.5 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	17.1	$F_{tuw} =$	25 k/in ²
screws in holes	J.5.5.1	16.7	$E =$	10,100 k/in ²
			$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	5.8	22.6	$0.00003 \lambda^2 - 0.032\lambda + 6.5$	169	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2	-	see F.4	169	$60,414/\lambda^2$	
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	5.8	10.3	$7.4 - 0.156\lambda$	31	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	5.8	10.3	$7.4 - 0.156\lambda$	23.5	$87/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	5.8	32.1	$7.4 - 0.050\lambda$	74	$271/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	5.8	22.6	$6.3 - 0.025\lambda$	169	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	5.8	55.3	$7.3 - 0.210\lambda^{1/2}$	573	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	5.8	51.3	$7.4 - 0.031\lambda$	118	$433/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	8.6	36.1	$9.8 - 0.031\lambda$	157	$767/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	8.6	6.7	$9.8 - 0.167\lambda$	39	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	8.6	80.9	$9.8 - 0.014\lambda$	353	$1,719/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$11.0 - 0.494\lambda^{1/2}$	166.0	$7.3 - 0.210\lambda^{1/2}$	537	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	51.3	see B.5.5.5	157	$433/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	3.5	54.1	$4.4 - 0.018\lambda$	162	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	3.5	22.5	$4.4 - 0.044\lambda$	67	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	3.5	97.2	$5.8 - 0.024\lambda$	162	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	3.5	54.1	$4.4 - 0.018\lambda$	162	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-12W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5083 - H116	B928 0.125 to 1.500 in. thick
axial tension stress on net effective area	D.2b	20.5	5083 - H32	B209 0.125 to 1.500 in. thick
axial tension stress on gross area	D.2a	10.9	5083 - H321	B209 0.125 to 1.500 in. thick
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	12.3	$F_{tyw} =$	18 k/in ²
<u>Bearing</u>			$F_{cyw} =$	18 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	41.0	$F_{tuw} =$	40 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	27.3	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	26.7	$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	10.9	21.5	$0.00010 \lambda^2 - 0.089\lambda + 12.8$	121	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2	-	see F.4		121	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	10.9	8.5	$14.7 - 0.440\lambda$	22	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	10.9	8.5	$14.7 - 0.440\lambda$	16.7	$122/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	10.9	26.7	$14.7 - 0.141\lambda$	52	$382/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	10.9	21.5	$12.4 - 0.068\lambda$	121	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	10.9	43.2	$14.3 - 0.511\lambda^{1/2}$	327	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	10.9	42.7	$14.7 - 0.088\lambda$	83	$611/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	16.4	35.9	$19.5 - 0.088\lambda$	111	$1,085/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	16.4	6.7	$19.5 - 0.472\lambda$	28	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	16.4	80.4	$19.5 - 0.039\lambda$	249	$2,431/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$21.4 - 1.203\lambda^{1/2}$	106.3	$14.3 - 0.511\lambda^{1/2}$	327	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	42.7	see B.5.5.5	111	$611/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	6.5	45.0	$8.9 - 0.052\lambda$	114	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	6.5	18.8	$8.9 - 0.124\lambda$	48	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	6.5	74.0	$11.5 - 0.067\lambda$	114	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	6.5	45.0	$8.9 - 0.052\lambda$	114	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_p/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-13W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5086 - H34	B209 0.009 to 1.000 in. thick
axial tension stress on net effective area	D.2b	17.9	5086 - H34	B210 0.010 to 0.450 in. thick
axial tension stress on gross area	D.2a	8.5		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	10.8	$F_{tyw} =$	14 k/in ²
<u>Bearing</u>			$F_{cyw} =$	14 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	35.9	$F_{tuw} =$	35 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	23.9	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	23.3	$k_t =$	1

		λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$
<u>Axial Compression</u> - member buckling	E.2	kL/r	8.5	21.9	$0.00006 \lambda^2 - 0.059\lambda + 9.8$	138	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2		-	see F.4	138	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	8.5	9.2	$11.2 - 0.292\lambda$	25	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	8.5	9.2	$11.2 - 0.292\lambda$	19.1	$107/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	8.5	28.7	$11.2 - 0.094\lambda$	60	$333/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	8.5	21.9	$9.5 - 0.046\lambda$	138	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	8.5	47.6	$11.0 - 0.360\lambda^{1/2}$	416	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	8.5	46.0	$11.2 - 0.058\lambda$	96	$534/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	12.7	36.3	$14.8 - 0.058\lambda$	128	$946/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	12.7	6.7	$14.8 - 0.313\lambda$	32	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	12.7	81.4	$14.8 - 0.026\lambda$	286	$2,120/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$16.5 - 0.847\lambda^{1/2}$	126.7	$11.0 - 0.360\lambda^{1/2}$	416	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	46.0	see B.5.5.5	127	$534/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	5.1	48.5	$6.8 - 0.034\lambda$	131	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	5.1	20.2	$6.8 - 0.082\lambda$	55	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	5.1	82.4	$8.8 - 0.045\lambda$	131	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	5.1	48.5	$6.8 - 0.034\lambda$	131	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-14W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5086 - H116	B928 0.063 to 2.000 in. thick
axial tension stress on net effective area	D.2b	17.9	5086 - H32	B209 0.020 to 2.000 in. thick
axial tension stress on gross area	D.2a	8.5	5086 - H32	B210 0.010 to 0.450 in. thick
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	10.8	$F_{tyw} =$	14 k/in ²
<u>Bearing</u>			$F_{cyw} =$	14 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	35.9	$F_{tuw} =$	35 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	23.9	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	23.3	$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	8.5	21.9	$0.00006 \lambda^2 - 0.059\lambda + 9.8$	138	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2	-	see F.4		138	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	8.5	9.2	$11.2 - 0.292\lambda$	25	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	8.5	9.2	$11.2 - 0.292\lambda$	19.1	$107/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	8.5	28.7	$11.2 - 0.094\lambda$	60	$333/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	8.5	21.9	$9.5 - 0.046\lambda$	138	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	8.5	47.6	$11.0 - 0.360\lambda^{1/2}$	416	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	8.5	46.0	$11.2 - 0.058\lambda$	96	$534/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	12.7	36.3	$14.8 - 0.058\lambda$	128	$946/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	12.7	6.7	$14.8 - 0.313\lambda$	32	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	12.7	81.4	$14.8 - 0.026\lambda$	286	$2,120/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$16.5 - 0.487\lambda^{1/2}$	126.7	$11.0 - 0.360\lambda^{1/2}$	416	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	46.0	see B.5.5.5	127	$534/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	5.1	48.5	$6.8 - 0.034\lambda$	131	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	5.1	20.2	$6.8 - 0.082\lambda$	55	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	5.1	82.4	$8.8 - 0.045\lambda$	131	$50,264/\lambda^2$
Torsion - pipes and round or oval tubes	H.2.1	λ_D^*	5.1	48.5	$6.8 - 0.034\lambda$	131	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_p/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-15W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

Axial Tension	Section	F/Ω	5454 - H32	B209 0.020 to 2.000 in. thick
axial tension stress on net effective area	D.2b	15.9		
axial tension stress on gross area	D.2a	7.3		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	9.5	$F_{tyw} =$	12 k/in ²
<u>Bearing</u>			$F_{cyw} =$	12 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	31.8	$F_{tuw} =$	31 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	21.1	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	20.7	$k_t =$	1

	λ	F/Ω for λ ≤ λ ₁	λ ₁	F/Ω for λ ₁ < λ < λ ₂	λ ₂	F/Ω for λ ≥ λ ₂	
<u>Axial Compression</u> - member buckling	E.2	kL/r	7.3	22.2	$0.00004 \lambda^2 - 0.046\lambda + 8.3$	150	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2	-		see F.4	150	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	7.3	9.6	$9.5 - 0.228\lambda$	28	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	7.3	9.6	$9.5 - 0.228\lambda$	20.8	$98/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	7.3	30.0	$9.5 - 0.073\lambda$	65	$307/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	7.3	22.2	$8.1 - 0.036\lambda$	150	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	7.3	50.5	$9.3 - 0.291\lambda^{1/2}$	481	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	7.3	48.0	$9.5 - 0.046\lambda$	104	$491/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	10.9	36.4	$12.6 - 0.045\lambda$	139	$870/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	10.9	6.8	$12.6 - 0.244\lambda$	34	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	10.9	81.5	$12.6 - 0.020\lambda$	311	$1,950/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$14.0 - 0.684\lambda^{1/2}$	141.1	$9.3 - 0.291\lambda^{1/2}$	481	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	48.0	see B.5.5.5	138	$491/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	4.4	50.7	$5.7 - 0.027\lambda$	142	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	4.4	21.2	$5.7 - 0.064\lambda$	59	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	4.4	88.0	$7.4 - 0.035\lambda$	142	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	4.4	50.7	$5.7 - 0.027\lambda$	142	$38,665/\lambda^2$

$$*\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$$

$$^\dagger k_n = (1 + \lambda^{1/2}/35)^2$$

Table 2-16W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

<u>Axial Tension</u>	Section	F/Ω	5454 - H34	B209 0.020 to 1.000 in. thick
axial tension stress on net effective area	D.2b	15.9		
axial tension stress on gross area	D.2a	7.3		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	9.5	$F_{tyw} =$	12 k/in ²
<u>Bearing</u>			$F_{cyw} =$	12 k/in ²
bolts or rivets on holes	J.3.6a, J.4.6	31.8	$F_{tuw} =$	31 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	21.1	$E =$	10,100 k/in ²
screws in holes	J.5.5.1	20.7	$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression</u> - member buckling	E.2	kL/r	7.3	22.2	$0.00004 \lambda^2 - 0.046\lambda + 8.3$	150	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2	-	see F.4		150	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	7.3	9.6	$9.5 - 0.228\lambda$	28	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	7.3	9.6	$9.5 - 0.228\lambda$	20.8	$98/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	7.3	30.0	$9.5 - 0.073\lambda$	65	$307/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	7.3	22.2	$8.1 - 0.036\lambda$	150	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	7.3	50.5	$9.3 - 0.291\lambda^{1/2}$	481	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	7.3	48.0	$9.5 - 0.046\lambda$	104	$491/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	10.9	36.4	$12.6 - 0.045\lambda$	139	$870/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	10.9	6.8	$12.6 - 0.244\lambda$	34	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	10.9	81.5	$12.6 - 0.020\lambda$	311	$1,950/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$14.0 - 0.684\lambda^{1/2}$	141.1	$9.3 - 0.291\lambda^{1/2}$	481	$3,776/(\lambda k_n)\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	48.0	see B.5.5.5	138	$491/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	4.4	50.7	$5.7 - 0.027\lambda$	142	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	4.4	21.2	$5.7 - 0.064\lambda$	59	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	4.4	88.0	$7.4 - 0.035\lambda$	142	$50,264/\lambda^2$
Torsion - pipes and round or oval tubes	H.2.1	λ_D^*	4.4	50.7	$5.7 - 0.027\lambda$	142	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$

† $k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-17W
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (WELDED)

Axial Tension	Section	F/Ω	6005A - T61		B221 0.000 to 1.000 in. thick		
axial tension stress on net effective area	D.2b	12.3					
axial tension stress on gross area	D.2a	7.9					
<u>Shear or torsion</u>							
Shear or torsion rupture	G, H.2	7.4		$F_{tyw} =$	13 k/in ²		
<u>Bearing</u>				$F_{cyw} =$	13 k/in ²		
bolts or rivets on holes	J.3.6a, J.4.6	24.6		$F_{tuw} =$	24 k/in ²		
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	16.4		$E =$	10,100 k/in ²		
screws in holes	J.5.5.1	16.0		$k_t =$	1		
		λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$
<u>Axial Compression</u> - member buckling	E.2	kL/r	7.9	22.1	$0.00005 \lambda^2 - 0.053\lambda + 9.0$	144	$51,352/\lambda^2$
<u>Flexure</u> - lateral-torsional buckling	F.4	see F.4.2		-	see F.4	144	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	7.9	9.4	$10.3 - 0.259\lambda$	27	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	7.9	9.4	$10.3 - 0.259\lambda$	19.9	$103/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	7.9	29.4	$10.3 - 0.083\lambda$	62	$320/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	7.9	22.1	$8.8 - 0.041\lambda$	144	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	7.9	49.0	$10.2 - 0.325\lambda^{1/2}$	446	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	7.9	47.0	$10.3 - 0.052\lambda$	99	$513/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	11.8	36.4	$13.7 - 0.052\lambda$	133	$909/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	11.8	6.8	$13.7 - 0.278\lambda$	33	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	11.8	81.5	$13.7 - 0.023\lambda$	298	$2,037/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$15.2 - 0.764\lambda^{1/2}$	133.4	$10.2 - 0.325\lambda^{1/2}$	446	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	47.0	see B.5.5.5	133	$513/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	4.7	49.5	$6.2 - 0.030\lambda$	136	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	4.7	20.6	$6.2 - 0.073\lambda$	57	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	4.7	85.0	$8.1 - 0.040\lambda$	136	$50,264/\lambda^2$
<u>Torsion</u> - pipes and round or oval tubes	H.2.1	λ_p^*	4.7	49.5	$6.2 - 0.030\lambda$	136	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$